CH2M HILL. 1100 112th Avenue, Suite 400 Bellevue, WA 98004 USA



Attention: Mark Thompson, Ph.D., P.E.

Dear Mr. Thompson

<u>RE: Static and Dynamic Laboratory Tests on Samples from Port of Anchorage,</u> <u>Anchorage, US</u>

MEG Consulting Limited (M+EG) was requested to provide both static and dynamic laboratory testing services to CH2M HILL on samples for the Port of Anchorage project. The test program proposed by CH2M HILL is presented on Table 1. The focus of the laboratory testing was constant rate of strain (CRS) consolidation tests, static direct simple shear tests (DSS), consolidated undrained (CU) triaxial, and cyclic DSS tests. Complimentary classification tests were performed on samples for indexing. The classification tests consisted of water content, unit weight, particle size distribution, specific gravity and Atterberg limits. Testing will be discussed later in the report.

SAMPLE TRANSPORT AND GAMMA SCANS

The samples arrived at M+EG on May 23, 2012 via FEDEX. They arrived on two pallets and each pallet had four sample boxes containing nine 2.8-inch diameter Shelby tubes each, with the exception of one box that contained four 6-inch diameter Shelby tubes. The boxes were bolted down to the pallets and were strapped together (Figure 1). The inside of all the boxes was lined with Styrofoam padding creating a fairly snug fit for each Shelby tube (Figure 2) for protection during sample shipment.

CH2M HILL provided M+EG with a list of 19 samples for gamma scan imaging. The scans were performed and digital images of the negatives were provided to CH2M HILL to assess sample quality and determine the best locations for sample quality within each Shelby tube. Based on the scans, it was determined that sample quality varied from good quality to some highly disturbed sections. Due to these highly disturbed samples, an additional four Shelby tubes were scanned. The samples that were sent for gamma scans are indicated in Table 1 and the digital images of the gamma scans are presented in Appendix B1.

SAMPLE STORAGE, CUTTING AND EXTRUSION

The samples that were scheduled for testing were placed in a controlled environment for storage. The samples were stored in a commercial fridge where the temperatures ranged from 3° C and 8° C. Not all the samples could be placed in the controlled environment

due to the large volume of samples. The samples that were not scheduled for testing were placed in a temperature-controlled room and left in the shipping boxes.

Once the sections were determined where the samples were to be tested, the Shelby tubes were cut in order to extrude the sample for testing. The samples were placed into a cutting horse and slowly cut using a pipe cutter. The pipe cutter was rotated around the circumference of the Shelby tube while applying very little pressure to the blade. Once the Shelby tube was cut, the pipe cutter was removed and a wire saw was used to cut through the soil in order to isolate the sample. On average it took about 10 minutes to complete one cut. By inspection, a couple of the Shelby tubes were found to be slightly warped (Figure 3). The degree to which the samples were warped varied. The samples that were slightly warped could still be placed in the extruder, but the samples that were more warped would not fit into the extruder, and were unable to be extruded and tested.

During the cutting process it was also observed that some of the Shelby tubes had cutting edges that were bent and damaged. Depending on when this damage occurred during the in situ sampling process, the damaged/deformed section of the tube could have affected the condition of the sample as it passed into the tube during sampling (Figure 4 and Figure 5).

To extrude the sample, the cut section was placed in a vertically-aligned jack and the sample was extruded out of the Shelby tube in the same direction as the sampling push, in order to try to minimize possible disturbance. While the samples were being extruded, a couple samples were noted that were very disturbed and not possible to test (Figure 6). When samples of this type were encountered, CH2M HILL was notified and asked for instructions on how to proceed with each particular sample.

CLASSIFICATION/INDEX TESTS

Classification tests were performed to complement the more advanced tests. The water content and unit weight were determined for each specimen tested. The results are reported in Tables 3 and 4, which summarize sample details before and after testing, as well as the data for each individual test where multiple tests were performed.

One Atterberg limits and particle size distribution was performed on every sample scheduled for consolidation tests. For the particle size distribution, both sieve and hydrometer analyses were performed due to the fine grained nature of the samples. The results obtained from these tests were very consistent with each other and indicate that the majority of the samples tested consisted of material that classified between a silty CLAY with some sand and CLAY with some silt and sand. The results for the Atterberg limits are presented in Appendix B.3 and the grain size distribution results are in Appendix B.4. A specific gravity test was also performed on each sample. The specific gravity was used to calculate the void ratios for all the advanced tests.

CONSOLIDATION TESTS

A total of 26 consolidation tests were performed. Of the 26 tests, 24 were constant rate of strain tests (CRS) and 2 were load increment ratio tests (LIR). The two LIR consolidations were performed on samples that were also tested in the CRS equipment.

The LIR consolidations were used as a check for the CRS consolidations. Because of this and the length of performing a load – unload sequence on the LIR consolidometers, the samples were only consolidated to 3000 kPa. The load steps used for both LIR tests were 35 kPa, 70 kPa, 125 kPa, 250 kPa, 500 kPa, 1000 kPa, 1800 kPa and 3000 kPa. The results for the LIR tests are presented in Appendix B.6.

Throughout the project, a few loading schedules were used for the CRS consolidations. The first schedule required the sample to be consolidated to 1400 kPa, then unloaded to 1000 kPa, reloaded to 2800 kPa and, finally unloaded to 100 kPa. This loading sequence was used for the first two tests, at which time the loading sequence was changed to further define certain aspects of the consolidation curve. The second sequence used involved two steps; an initial load to 7000 kPa and unloading to 100 kPa. The increase of the consolidation pressure to 7000 kPa provided much better definition of the full consolidation curve, but was later modified to add an unload-reload sequence. The final schedule that was used on the majority of the samples was to consolidate the sample to 3000 kPa, unload to 100 kPa before finally loading to 7000 kPa. The results for the CRS consolidation tests are presented in Appendix B.7.

A maximum consolidation pressure of 7000 kPa was used as this was the limit that could be applied to the sample using a 5000 lb load cell. The loading stages were achieved at a strain rate of 0.8% per hour; a rate of 0.4% per hour was used for the unloading stages.

The sample preparation for both consolidation tests is the same. The soil sample is gradually trimmed to the correct diameter as the consolidation ring is slowly pushed into the sample. The final trimmed sample in the solid consolidation ring has a diameter of 2.5 inches, and is 1 inch high.

STATIC DIRECT SIMPLE SHEAR (DSS)

A total of 30 static DSS test were performed as part of the testing program. Two consolidation procedures were used for the DSS samples. The recompression technique was used to target specific over-consolidation ratios (OCR) while SHANSEP procedures also targeted a specific OCR and also helped reduce disturbance effects in the sample. A range of OCRs between 1 and 8.5 were tested.

A static DSS setup from GeoTAC in Houston was one of the pieces of equipment used to perform the required testing. The samples to be tested in this apparatus had to be trimmed slightly to a dimater of 66.5 mm in oder to fit into the shear rings. A sample height of 22.3 mm was used. The samples were placed in the DSS apparatus aand consolidated prior to shearing. Other tests were performed in a GDS setup, where the

samples have an initial height of 23.6 mm and a diameter of 72.6 mm. Details of the static DSS tests performed and the results are presented in Appendix B.8.

CONSOLIDATED UNDRAINED TRIAXIAL

A total of 19 consolidated triaxial tests were performed. In order to avoid trimming the samples, CH2M HILL requested that the testing be performed on samples with a diameter of 2.8 inches. The first couple of samples were tested with the saturation and consolidation stages lasting over a week. Due to the tight scheduling, it was decided that a smaller diameter sample (1.4 inch) be tested. This greatly decreased the amount of time needed to saturate and consolidate the sample. In order to help speed up the process, samples were prepared and setup to saturate connected to a back-pressure panel.

The majority of the testing was performed using SHANSEP procedures for consolidation testing with OCRs ranging between 1 and 8.8. The reconsolidation stage was performed using a k value of 0.55. Once the sample had completed consolidation, the sample was unloaded at a different k value to the final vertical and horizontal pressures. The final k value ranged between 0.55 and 1.40.

For the first sample tested at a k value greater than 1, the sample was lost because the top cap became disconnected from the piston as the vertical stress unloaded to a state of extension. Modifications were made to the triaxial setup and all further testing with k values of 1.13 and lower were performed without any additional complications. Of the four samples that required a k greater than 1.13, only one test was possible. At this high k value, equipment modifications would have been required to manage the tensions in the vertical loading system. IN discussions with CH2M HILL, it was decided to reduce the k value to 1.1 for the four tests. The results are presented in Appendix B.8.

CYCLIC AND POST-CYCLIC DIRECT SIMPLE SHEAR (DSS)

Cyclic DSS tests were scheduled for four samples, and each was to be tested at 4 different cyclic stress ratios (CSR). The first set of tests was performed on sample BH-003-12 ST11 with an effective vertical stress of 1000 kPa. These were tested at CSR values of 0.10, 0.15, 0.20, and 0.25. After the cyclic test was completed for each stress level, a post-cyclic direct simple shear test was performed.

CH2M Hill then advised that they required bender element shear wave velocity measurements to be performed beginning on the next set of tests.

The second set was originally scheduled for BH-003-12 ST 14, but because the Shelby tube was warped, the testing was changed to BH-003-12 ST16 (this is the same sample as for the set 3 tests). The sample was consolidated to a confining pressure of 1000 kPa and then a static bias of 120 kPa was applied and left to consolidate until the measured horizontal displacement was constant. At this point, the sample was tested at CSR values of 0.05, 0.10, 0.10 and 0.20. After the cyclic DSS test was complete, a post-cyclic DSS

test was performed ensuring the sample was taken to the initial static bias before static shearing was commenced. Bender element shear wave velocity measurements were taken prior to the application of the static bias in order ensure alignment of the elements.

Set 3 was consolidated to 1000 kPa and unloaded to 500 kPa creating an OCR of 2. As expected, by imposing an OCR, the sample reached a higher CSR at failure. CSR values of 0.20, 0.25, 0.35 and 0.40 were used and each test was also followed by a post-cyclic DSS. Bender element shear wave velocity measurements were takes once the sample had been unloaded to 500 kPa.

The testing parameters for the last set were identical to set one but each test was followed by a post-cyclic DSS. The results of the Cyclic DSS, post-cyclic DSS and bender element shear wave velocity measurements are presented in Appendices B10, B11 and B12, respectively.

CLOSURE

In providing the testing service, M+EG has followed generally accepted procedures defined by the ASTM standards and the existing state-of-practice, at the same time addressing specific conditions requested by the Client. The results obtained, however, will depend on the quality of the samples tested. The decision as to which samples to test is the sole responsibility of the Client. As such, M+EG is not able to provide any guarantees as to the representative nature of the results obtained.

M+EG has executed the laboratory tests in a manner consistent with a level of care and skill ordinarily exercised by members of the engineering and geosciences professions currently practicing in British Columbia, subject to the sample quality, time limits and physical constraints applicable to this project. No other warranty, expressed or implied is made.

Sincerely, MEG Consulting Limited

Paul Sully Laboratory Manager

Reviewed By:

John P. Sully, Ph.D., P. Eng. Principal

FIGURES



Figure 1: sample shipping and packaging showing boxes bolted down to pallets and strapped together



Figure 2: padding and lining of sample boxes



Figure 3: Slightly warped Shelby tube



Figure 4: Possible disturbance caused by a bent cutting edge



Figure 5: Bent cutting edge



Figure 6: Disturbed sample after extrusion

August 2012

TABLES

Marine + Earth MEG Consulting Limited																																			
Client: Project Nº:	nt: CH2M Hill Boring N°: Various For week:														_	1		of 1																	
Laboratory Test Schedule																																			
SAMPLE CLASSIFICATION SHEAR STRENGTH CONSOLIDATION DYNAMIC TEST																																			
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Sample No.	Soil Type	Sample Type	Bottom Depth (m)	Water Content	Unit Weight	Atterberg Limits	Sieve % < # 200 siava siza	Hydrometer	Carbonate Content	Organic Content	Specific Gravity Max / Min Density	Pocket Penetrometer	CU Triaxial	Direct Simple Shear	LIR Oedometer	CRS Oedometer	Pressure (kPa)	Bander Flements			Strain-Controlled DSS		Stress-Controlled DSS		Post-Cyclic DSS			Post-Cyclic Consolidation		X-ray	Comments				
BH-003-12 ST-2		SH	28.35	x	X	x	(x			x		x	х	х	х	х		х	х	2800 kPa											-	$\left - \right $	х	
ST-3		SH	29.26	Х	Х	X X	(X			х		Х	Х	Х					Х	2800 kPa													X	
ST-4		SH	29.87	X	X	XX	< /	X			X	-	Š	X						X	2800 kPa		-		_		_			-		-	-	X	
ST-6		SH	30.78	X	X		κ κ	X			X		Ş	X X						X X	7000 kPa 7000 kPa					x	x x	r x	×	Y		–	\vdash	X	
ST-0		SH	35.33	x	x	x x	Ì.	x			x		\sim	^					х	x	1000 11 4						^ ^	` î		^		-	\square		
ST-9		SH	38.40	X	Х	XX	(X			X		Χ	X						X	7000 kPa													Х	
ST-10		SH	39.01	X	X	XX	(X			X		X	Х						X	7000 kPa					v	~ `	<i>,</i> ,		v	v	v	v	X	ŀ
ST-12		SH	40.54	x	x	x	<	x			x		x	x						x	7000 kPa					^	^ ^	` ^	1	^	^	^	^	Ŷ	
ST-13		SH	41.45				-														7000 kPa													X	
ST-14		SH	42.06																		70001 0													X	ļ
ST-15 ST-16		SH SH	42.98	X	X	X		Y			X		X	х						X	7000 kPa 7000 kPa							\rightarrow	$ \downarrow$	\checkmark	\checkmark	┢	\checkmark	X	
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BH-001-12																																			
ST-4		SH	21.95	X	X	XX	<u> </u>	X			X	_								X	7000 kPa				_				_	_					ŀ
ST-13		SH	29.26	x	x	x	È.	x			x		x	x	x					x	7000 kPa											-	+	х	
ST-14		SH	29.87	X	X	X	-				X		X	X	X	х																		X	
ST-15		SH	31.09	Х	х	X	(X			X		Х	Х						х	7000 kPa						_					<u> </u>		Х	
BH-004-12																												_					+		[
ST-3		SH	19.81	Х	х	X X	ĸ	Х			х									х	7000 kPa											-			
ST-7		SH	24.69	X	Х	XX	(Х			X			X						X	7000 kPa														ļ
ST-9 ST-10		SH	27.74	X	X	X	K	X	-	$\left \right $	x			X	X	X				X	7000 kPa	_	-	\vdash	-	+	-	_	-	+	-	+	+	X	
ST-11		SH	29.26	X	х	x x	(x			х		×	х	х					х	7000 kPa											-	+	x	
ST-13		SH	30.78	Х	Х	XX	(X			Х		Х							Х	7000 kPa														
BH-005-12				_																						+		_				-	-		
ST-3		SH	15.24	x	x	x	ĸ	x			x			х	х					х	7000 kPa									_		-	+	-	
ST-8		SH	19.20	Х	Х	X	(X			X									Х	7000 kPa													Х	
ST-10		SH	21.95	-	v			v	-	$\left \right $	v			v	v	v				v	7000 kPa		-		_	+	_	_	-	+	-	⊢	\vdash	X	
ST-11 ST-12		SH	22.80	-	^	<u> ^</u> '	<u> </u>	^	-		^	1		^	^	^				^			-	\vdash	+	+			-	-	-	+	+	Ŷ	
ST-13		SH	24.38	Х	X	X					X									х	7000 kPa														
ST-16		SH	26.52			X	+	+			x	<u> </u>	_								7000 kPa	_	+		+	+	+		+	+		⊢	\vdash		
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APPENDIX A

GEOTECHNICAL LABORATORY

GENERAL TESTING PROCEDURES

A.1 Gamma-ray

Prior to testing CH2M Hill provide a list of 23 shelbey tube sample to scan. Photograph negatives and digital files were produced and provided to CH2M Hill to provide input on test locations and also to help asses sample conditions and disturbance. The digitized negatives are provided in Appendix B.1.

A.2 Moisture Content and Total Unit Weights

Water (or moisture) contents (*w*) are determined from measured total and dry weights of specimens taken from the soil samples. Measurements are performed in accordance with the procedures described in ASTM D 2216. Water content measurements are performed on all samples to be used for advanced tests.

The measurements of total (γ_t) and dry (γ_d) unit weight of the recovered soil samples are determined in accordance with BS 1377 (BSI, 1990 – no ASTM standard available). The unit weight values are reported in units of kN/m³. The dry, total and submerged unit weights are used to calculate the different stress profiles in a soil mass that are used for engineering calculations. The values are inter-related as given by:

$$\gamma_{d} = \gamma_{t} / (1 + w)$$

 $\gamma' = \gamma_{t} - \gamma_{w}$

where w is the water content expressed as a decimal.

A.3 Atterberg Limits and Moisture Content

The Atterberg limit tests are performed directly on the soil samples using the multipoint test. The liquid (LL%) and plastic (PL%) limits are determined using the test procedures described in ASTM D 4318. The plasticity (PI%) index is defined as:

$$PI\% = LL\% - PL\%$$

The liquidity index (LI) is defined as:

LI = (w% - PL%)/ Plasticity Index%

A.4 Grain Size Distribution (Sieve + Hydrometer)

Sieve analyses are performed in accordance with the procedures described in ASTM D 422. The proportion of fines (silt and clay) in a specimen is determined by washing the material through the #200 (75 μ m) sieve, and computing the percentage passing. Results for grain size distribution analyses are presented on a semi-logarithmic plot with grain size (log) versus percentage passing by weight finer than the grain size.

The hydrometer test is used to determine the grain size distribution of fine-grained materials by a sedimentation method. The test procedures adopted are described in detail in ASTM D 422. The test allows the determination of silt and clay percentages of the fine grained portion of a sample. The results of the particle size and fines content determinations are combined with the results of the hydrometer tests to provide a profile of soil constituents.

A.5 Specific Gravity

Specific gravity (G_s) measurements of the soil particles are performed according to the procedure detailed in ASTM D 854. The specific gravity is used to calculate the void ratio of the soils based on the dry unit weights. The specific gravity is also necessary for interpreting the hydrometer test data.

A.6 One-Dimensional Consolidation Using Standard Load Increment (LIR)

One-dimensional consolidation (oedometer) tests have been performed on selected samples to investigate the compressibility characteristics and stress history of the soil. Once the sample is prepared, placed in the testing apparatus, and fully saturated, loads are applied incrementally. Loads are applied sequentially, the magnitude of which is doubled at each load step, or using specified load increments. Time, applied normal load, and vertical displacement readings are recorded and used to compute the void ratio-effective vertical pressure relationship. Detailed descriptions of the testing procedures are provided in ASTM D 2435.

A.7 One-Dimensional Consolidation Using Constant Rate of Strain Loading (CRS)

One-dimensional consolidation tests are also performed using constant rate of strain loading condition. The specimen is prepared, placed in the testing apparatus, flushed and saturated using de-aired water. Axial loads are applied to produce axial strain at a constant rate. Based on the sample characteristics, a strain rate of 0.8% per hour was used during the loading stages and 0.4% per hour was used for unloading. The constant strain rate is selected to target a maximum excess pore pressure of less than 10%, as recommended in the ASTM standard (ASTM D 4186). Applied load, vertical displacement and pore pressure are recorded and used to compute the void ratio-effective vertical pressure relationship, excess pore pressure (Δu) and coefficient of consolidation (c_v) plots. Detailed descriptions of the testing procedures are provided in ASTM D 4186.

A.8 Consolidated Undrained Triaxial

Consolidated-undrained (CU) triaxial compression tests provide undrained shear strength characteristics, stress-strain relationships and stress path for the soil specimens tested. A soil sample is prepared and placed in a rubber membrane inside the triaxial cell. The sample is then saturated under a back-pressure ranging between 345 kPa and 483 kPa.

After the saturation stage, the sample is consolidated anisotropically with a specified k_0 provided by the client (i.e. $k_0 = 0.5$). The specimen is then loaded uniaxially to failure at a constant rate of strain under undrained conditions. Detailed procedures for sample preparing, saturation, consolidation and shearing are described in ASTM D 4767.

The following plots are prepared for each test:

- Cell pressure versus pore water pressure during saturation.
- Volumetric strain versus time during consolidation.
- Shear stress (τ) versus axial strain (γ).
- Deviator stress versus axial strain (*γ*).
- Graph of stress paths.

For the Port of Achorage, consolidation was performed at 0.4% per hour for loading stages and 0.2 % per hour for unloading. Shear was performed at 0.4% per hour. Prior to placing in the load frame the samples were prepared and hooked up to a panel to allow for saturation under a backpressure of at least 345kPa with an effective stress of 20kPa. At least one pore volume of water was passed through the sample prior to backpressure saturation.

A.9 Static Direct Simple Shear (DSS) Tests

Direct simple shear (DSS) test is performed under constant volume conditions by deforming a specimen at a controlled strain after the specimen is consolidated to the estimated in situ effective vertical stress and OCR condition. Detailed testing procedures for the DSS tests are described in ASTM D 6528.

The following plots are prepared for each test:

- Shear stress (τ/σ'_{vc}) versus effective vertical stress (σ'_v) .
- Shear stress (τ) versus shear strain (γ).
- Change of vertical stress $(\sigma_{vc} \sigma_v)$ versus shear strain (γ).

A.10 Stress-Controlled Cyclic DSS Tests

Stress-controlled cyclic direct simple shear (DSS) tests are performed under constant volume conditions according to the following general procedure:

a) Each test specimen is consolidated to an effective vertical consolidation stress (σ'_{vc}) equal to the targeted vertical stress condition (σ'_v) . This consolidation process is allowed to continue for about one log cycle of time or 24 hours, whichever occurred first, past the time for the end of primary consolidation (t_{100}) to ensure that the K_0 condition is developed. If the soil in the field are

overconsolidated, the sample can be unloaded to produce an identical overconsolidation ratio (OCR).

b) Following the consolidation process, cyclic horizontal shear stresses (τ_{cyc}) are applied sinusoidally at an amplitude providing an average cyclic stress ratio (τ_{cyc}/σ_{ν}). The τ_{cyc} is applied at constant volume with a specified frequency (i.e. 0.1 Hz) for 100 cycles or until about 5% single amplitude strain is reached, whichever occurs first. If after 100 loading cycles, neither 100% increase in pore pressure has occurred nor 5% single amplitude strain is reached, then the test is stopped. Since the test is performed at constant volume, the pore pressure in the sample is estimated by monitoring the changes in the vertical stress ($\Delta \sigma_{\nu}$) applied to the specimen during cycling.

The following plots are prepared for each test:

- Average cyclic stress ratio (τ_{cyc}/s_u) versus log number of cycles.
- Vertical stress ratio $(\Delta \sigma_v / \sigma'_{vc})$ versus log number of cycles.
- Shear stress versus shear strain (stress-strain loops).
- Shear stress versus effective vertical stress

The vertical displacements for each consolidation stage have been monitored and recorded and are available upon request.

A.11 Post-cyclic Monotonic DSS Tests

Once the sample has been tested under cyclic loading and without allowing any consolidation or dissipation of the final excess pore pressure condition, the sample is statically sheared at constant volume and at a constant strain rate (i.e. 5%/hour) in accordance with the general procedure described in ASTM D 6528.

The following plots are prepared for each test:

- Shear stress (τ/σ'_{vc}) versus effective vertical stress (σ'_v) .
- Shear stress (τ) versus shear strain (γ).

A.12 Bender Element Velocity Measuring

Special end platens with embedded bender elements are used with the electro-mechanical DSS equipment to measure shear (S) wave velocities. The bender element array and data acquisition system were also designed and built by GDS.

The principle of the velocity measurement using bender elements is based on the time that a user-defined signal (sinusoidal, square, etc) is transmitted from one platen to the other. The signal is produced by the electrical excitation of a bender element The GDS bender element monitoring system (BEMS) is used to measure the shear wave velocity of the DSS samples immediately after initial consolidation to the in situ stress condition prior to shearing. The bender element signal generation and data acquisition is controlled by the GDS BEMS software package.

A plot of the transmitted and received signal with time is presented for each test performed. The shear wave velocity is calculated by using the travel time for the first arrival between the top and bottom of the sample. No data filtering / interpretation techniques are applied.

APPENDIX B.1

GAMMA-RAY RESULTS





Port of Anchorage CH2M





















Borehole: BH 003-12

CH2M







12-MTS-009



Port of Anchorage





















Borehole: BH 003-12

Port of Anchorage

CH2M









Port of Anchorage
Borehole: BH 004-12









Borehole: BH 005-12





Port of Anchorage CH2M	12-MTS-009 Dynamic Laboratory Tests
Borehole: BH 005-12	





Borehole: BH 004-12



Sample No. ST- 10 (28.04-28.65m) Top



Sample No. ST- 10 (28.04-28.65m) Bottom



Port of Anchorage
CH2M
Dynar

12-MTS-009 Dynamic Laboratory Tests

Borehole: BH 005-12

Sample No. ST-11 (22.25-22.86m) Top



Sample No. ST-12 (22.86-23.46m) Top



Port of Anchorage CH2M			12-MTS-009 Dynamic Laboratory Tests
Borehole: BH 005-12			
Sample No. ST-11 (22.25-22.86m) Bottom			
		MEG CONSULTING MAY29 2012 PO A	
Sample No. ST-12 (22.86-23.46m) Bottom	35 40	50 ST 12	60



Borehole: BH 001-12



Sample No. ST-14 (29.26-29.87m) Top



APPENDIX B.2

WATER CONTENT & UNIT WEIGHT



MEG TECHNICAL SERVICES

(A Division of MEG Consulting Limited)

Project:		Port o	f Anchorage	9				Project N	lo.: 12-MTS-009			
Location:		Ancho	orage , US					Date:		J	une 4, 201	2
Borehole:		BH-00)1-12					Page:		1	of	4
Sample №	Depth (m)	Tin №	Wt. of tare (TW)	TW+ Wet weight	TW+ Dry weight (a)	Water Content	Sample Diameter (mm)	Sample Height	Sample Weight	Volume	Total Unit Weight (kN/m ³)	Dry Unit Weight (kN/m ³)
BH-001-12 ST-4	21.88	55	24.27	63.31	53.98	31.4	63.5	25.4	144 61	80.44	17.64	13.42
BH-001-12 ST-7	23.69	93	23.68	51.93	46.16	25.7	63.5	25.4	159.42	80.44	19.44	15.47
BH-001-12 ST-13	29.14	11	32.92	81.53	71.52	25.9	63.5	25.4	162.38	80.44	19.80	15.73
BH-001-12 ST-14	29.72	24	24.03	138.93	115.58	25.5	66.4	22.4	150.53	77.57	19.04	15.17
BH-001-12 ST-15	30.94	69	23.86	49.47	45.33	19.3	63.5	25.4	165.52	80.44	20.19	16.92
Performed By:			M	J	Checked	By:	P	S	Approved	l By:	JF	rs
Date:		June 4,	2012	Date:		August 2	24, 2012	Date:		August 2	27, 2012	



e + Earth

MEG TECHNICAL SERVICES

(A Division of MEG Consulting Limited)

Project:		Port o	f Anchorage	Э				Project N	t No.: 12-MTS-009				
Location:		Ancho	orage , US					Date:		J	une 4, 201	2	
Borehole:		BH-00)3-12					Page:		2	of	4	
Sample №	Depth	Tin №	Wt. of tare (TW)	TW+ Wet weight	TW+ Dry weight	Water Content	Sample Diameter	Sample Height	Sample Weight	Volume	Total Unit Weight	Dry Unit Weight	
BH-003-12 ST-2	28 29	13	24.82	104.90	90.25	22.4	63.5	25.4	163.99	80 44	20.00	16.34	
BH-003-12 ST-3	29.20	43	24.02	141 88	115.85	22.4	63.5	25.4	170.49	80.44	20.00	16.20	
BH-003-12 ST-4	29.81	77	33.83	185 13	154 27	25.6	63.5	25.4	159.99	80.44	19.51	15.53	
BH-003-12 ST-5	30.73	42	33.74	43.22	40.90	32.4	63.5	25.4	149.39	80.44	18.22	13.76	
BH-003-12 ST-6	30.73	28	24.00	45.44	40.62	29.0	63.5	25.4	153.99	80.44	18.78	14.56	
BH-003-12 ST-7	35.33	44	33.27	58.06	53.04	25.4	63.5	25.4	160.53	80.44	19.58	15.61	
BH-003-12 ST-9	38.30	70	32.89	81.43	72.28	23.2	63.5	25.4	165.44	80.44	20.18	16.37	
BH-003-12 ST-10	38.96	71	25.68	128.13	107.42	25.3	63.5	25.4	165.00	80.44	20.12	16.05	
BH-003-12 ST-12	40.48	111	33.12	104.25	90.88	23.1	63.5	25.4	162.51	80.44	19.82	16.09	
BH-003-12 ST-15	42.82	64	33.38	83.95	74.85	21.9	63.5	25.4	159.92	80.44	19.50	15.99	
BH-003-12 ST-16	42.98	71	25.67	48.09	43.27	27.4	63.5	25.4	159.06	80.44	19.40	15.23	
Performed By:			M	J	Checked	By:	P	S	Approved	By:	JF	PS	
Date:			June 4,	2012	Date:		August 2	24, 2012	Date:		August 2	27, 2012	



MEG TECHNICAL SERVICES

(A Division of MEG Consulting Limited)

Project:		Port o	f Anchorage	9				Project N	lo.: 12-MTS-009			
Location:		Ancho	orage , US					Date:		J	une 4, 201	2
Borehole:		BH-00	4-12					Page:		3	of	4
Sample №	Depth (m)	Tin №	Wt. of tare (TW) (g)	TW+ Wet weight (g)	TW+ Dry weight (g)	Water Content (%)	Sample Diameter (mm)	Sample Height (mm)	Sample Weight (g)	Volume (cm ³)	Total Unit Weight (kN/m³)	Dry Unit Weight (kN/m³)
BH-004-12 ST-3	19.80	24	33.04	62.54	57.09	22.7	63.5	25.4	165.32	80.44	20.16	16.44
BH-004-12 ST-7	24.62	28	24.00	45.34	40.97	25.8	63.5	25.4	162.48	80.44	19.82	15.76
BH-004-12 ST-9	27.67	67	24.04	61.58	53.52	27.3	63.5	25.4	158.70	80.44	19.35	15.20
BH-004-12 ST-11	29.19	93	23.68	59.93	52.79	24.5	63.5	25.4	160.29	80.44	19.55	15.70
BH-004-12 ST-13	30.63	81	24.07	43.59	39.80	24.1	63.5	25.4	163.06	80.44	19.89	16.02
Performed By:		8	M	J	Checked I	By:	P	S	Approved	d By:	JF	PS
Date:			June 4,	2012	Date:		August 2	24, 2012	Date:		August 2	27, 2012



MEG TECHNICAL SERVICES

(A Division of MEG Consulting Limited)

Project:		Port o	f Anchorage	Э				Project N	lo.: 12-MTS-009			
Location:		Ancho	orage , US					Date:		J	une 4, 201	2
Borehole:		BH-00)5-12					Page:		4	4 of 4	
Sample №	Depth (m)	Tin №	Wt. of tare (TW) (g)	TW+ Wet weight (g)	TW+ Dry weight (g)	Water Content (%)	Sample Diameter (mm)	Sample Height (mm)	Sample Weight (g)	Volume (cm ³)	Total Unit Weight (kN/m³)	Dry Unit Weight (kN/m³)
BH-005-12 ST-3	14.83	17	24.91	55.38	49.78	22.5	63.5	25.4	164.15	80.44	20.02	16.34
BH-005-12 ST-8	19.20	80	23.60	141.34	116.38	26.9	63.5	25.4	158.50	80.44	19.33	15.23
BH-005-12 ST-11	22.53	59	25.28	51.36	46.20	24.7	63.5	25.4	164.35	80.44	20.04	16.08
BH-005-12 ST-13	24.31	81	24.07	57.39	51.02	23.6	63.5	25.4	160.74	80.44	19.60	15.86
Performed By:		I	M	J	Checked	By:	P	S	Approved	l By:	JF	2S
Date:			June 4,	2012	Date:		August 2	24, 2012	Date:	-	August 2	27, 2012

APPENDIX B.3

LIQUID LIMIT, PLASTIC LIMIT, AND PLASTICITY INDEX



Classification of the material :

(A Division of MEG Consulting Limited)

Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)











Classification of the material :

(A Division of MEG Consulting Limited)

Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)















Marine + Earth

Geosciences



Classification of the material : CL











Classification of the material : CL







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : <u>CL</u>







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL

100 % with respect to the total of the material smaller than sieve No. 40





Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)



			LIQU	ID LIMI						PLA	ASTICL	IMII		
TIN No.	Tare + Weight of Wet Soil (g)	Tare + Weight of Dry Soil (g)	Weight of Tin (g)	Weight of Water (g)	Weight of Dry Soil (g)	Water Content (%)	No. of Blows	TIN No.	Tare + Weight of Wet Soil (g)	Tare + Weight of Dry Soil (g)	Weight of Tin (g)	Weight of Water (g)	Weight of Dry Soil (g)	Water Content (%)
24A	51.03	45.33	34.71	5.70	10.62	53.7	38	57	29.92	28.81	23.98	1.11	4.83	23.0
93	38.77	33.38	23.68	5.39	9.70	55.6	31	62	30.51	29.49	24.98	1.02	4.51	22.6
100	46.20	41.26	32.58	4.94	8.68	56.9	28							
2A	47.69	42.22	33.05	5.47	9.17	59.7	22							
94	45.83	40.68	32.48	5.15	8.20	62.8	18							

Classification of the material : MH

0/ with respect to the total of the material amplies then give N













Classification of the material : CH







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL













Classification of the material : CL







Classification of the material :

(A Division of MEG Consulting Limited)

Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)

















Classification of the material : CL









Classification of the material :





CL













Classification of the material : CL













Classification of the material : CL







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL













Classification of the material : CL







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL







Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)



Marine + Earth

Geosciences



Classification of the material : CL





Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)



			LIQU	ID LIM	Т			PLASTIC LIMIT						
TIN No.	Tare + Weight of Wet Soil (g)	Tare + Weight of Dry Soil (g)	Weight of Tin (g)	Weight of Water (g)	Weight of Dry Soil (g)	Water Content (%)	No. of Blows	-on NIT	Tare + Weight of Wet Soil (g)	Tare + Weight of Dry Soil (g)	Weight of Tin (g)	Weight of Water (g)	Weight of Dry Soil (g)	Water Content (%)
82	35.11	32.67	25.12	2.44	7.55	32.3	35	152	26.11	25.12	20.03	0.99	5.09	19.4
67A	35.95	32.94	24.06	3.01	8.88	33.9	27	154	26.73	25.62	19.85	1.11	5.77	19.2
25	43.22	41.01	34.67	2.21	6.34	34.9	20							
60	46.72	43.01	32.58	3.71	10.43	35.6	18							

Classification of the material : CL






(A Division of MEG Consulting Limited)

Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : <u>CL</u> 100 % with respect to the total of the material smaller than sieve No. 40







(A Division of MEG Consulting Limited)

Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL

100 % with respect to the total of the material smaller than sieve No. 40







Classification of the material :

(A Division of MEG Consulting Limited)





Marine + Earth

Geosciences



CL 100 % with respect to the total of the material smaller than sieve No. 40





(A Division of MEG Consulting Limited)

Liquid Limit, Plastic Limit and Plasticity Index of Soils (ASTM D 4318)





Classification of the material : CL

100 % with respect to the total of the material smaller than sieve No. 40





APPENDIX B.4

GRAIN SIZE DISTRIBUTION (SIEVE & HYDROMETER) ANALYSIS













































APPENDIX B.5

SPECIFIC GRAVITY



(A Division of MEG Consulting Limited)

Project:	Port of Ancl	norage		Project No.: 12-MTS-009		-009			
Location:	Anchorage, US				Date: June 22, 2012		2012		
Borehole:	BH-001-12								
Sample Number	Depth (m)	Volumetric flask No.	Weight of flask and soil (g)	Weight of flask, water and soil (g)	Weight of dry solid (g)	Temperature (°C)	Specific Gravity Gs		
BH-001-12 ST-4	21.88	7	213.60	688.72	36.81	20	2.74		
BH-001-12 ST-7	23.69	6	167.02	692.99	44.06	25	2.76		
BH-001-12 ST-13	29.19	4	213.07	689.48	36.45	20	2.74		
BH-001-12 ST-14	29.80	7	217.58	697.04	50.67	20	2.67		
BH-001-12 ST-15	31.02	5	210.24	689.15	35.78	20	2.75		
Comr	Comments :								
Prepared by: MJ			Checked by: PS Approved by: JPS			5			
Date: August 24, 2012			Date: August 26, 2012 Date: August			August 27	, 2012		



(A Division of MEG Consulting Limited)

Project:	Port of Anch	norage		Project No.: 12-MTS-009		-009		
Location:	Anchorage, US				Date: June 22, 2012		2012	
Borehole:	BH-004-12							
Sample Number	Depth (m)	Volumetric flask No.	Weight of flask and soil (g)	Weight of flask, water and soil (g)	Weight of dry solid (g)	Temperature (°C)	Specific Gravity Gs	
BH-004-12 ST-3	19.80	6	210.47	687.68	35.30	20	2.71	
BH-004-12 ST-7	24.62	6	216.30	696.77	49.32	22	2.83	
BH-004-12 ST-9	27.67	7	214.78	695.16	47.86	22	2.74	
BH-004-12 ST-11	29.19	5	214.71	696.06	46.93	22	2.83	
BH-004-12 ST-13	30.72	5	212.42	694.75	44.64	21	2.86	
Comr	Comments :							
Prepared by: MJ			Checked by:	PS	Approved by: JPS			
Date: August 24, 2012			Date:	August 26, 2012	Date: August 27, 2012			



(A Division of MEG Consulting Limited)

Project:	Port of Anch	norage		Project No.: 12-MTS-009		-009		
Location:	Anchorage, US				Date: May 30, 2012		2012	
Borehole:	BH-003-12							
Sample Number	Depth (m)	Volumetric flask No.	Weight of flask and soil (g)	Weight of flask, water and soil (g)	Weight of dry solid (g)	Temperature (°C)	Specific Gravity Gs	
BH-003-12 ST-2	28.29	6	246.37	715.36	79.37	22	2.72	
BH-003-12 ST-3	29.20	5	209.19	692.23	41.41	22	2.71	
BH-003-12 ST-4	29.81	6	221.56	699.96	54.58	22	2.75	
BH-003-12 ST-5	30.73	6	206.73	690.46	39.75	22	2.74	
BH-003-12 ST-6	31.29	7	216.98	696.94	50.06	24	2.77	
BH-003-12 ST-7	35.33	4	207.51	691.15	39.54	24	2.77	
BH-003-12 ST-9	38.30	5	207.28	690.96	39.40	24	2.71	
BH-003-12 ST-10	38.86	7	207.58	690.40	40.66	24.0	2.61	
BH-003-12 ST-12	40.54	5	219.53	698.91	51.75	25.0	2.79	
BH-003-12 ST-15	42.98	7	217.94	697.04	50.99	25.0	2.73	
BH-003-12 ST-16	43.52	6	206.89	690.29	39.91	24	2.69	
Comments :								
Prepared by	: N	VJ	Checked by:	PS	Approved by: JPS			
Date: June 23, 2012			Date:	July 5, 2012	Date: July 6,2012			



(A Division of MEG Consulting Limited)

Project:	Port of Ancl	norage		Project No.: 12-MTS-009		-009	
Location:	Anchorage, US				Date: June 22, 2012		2012
Borehole:	BH-005-12						
Sample Number	Depth (m)	Volumetric flask No.	Weight of flask and soil (g)	Weight of flask, water and soil (g)	Weight of dry solid (g)	Temperature (°C)	Specific Gravity Gs
BH-005-12 ST-3	14.83	6	208.78	691.92	41.80	21	2.83
BH-005-12 ST-8	19.06	4	219.01	698.41	50.72	21	2.74
BH-005-12 ST-11	22.53	7	216.71	696.98	49.79	19	2.74
BH-005-12 ST-13	24.31	6	218.05	697.54	50.68	19	2.73
BH-005-12 ST-16	26.44	5	218.35	698.56	50.57	21	2.75
Comr	nents :						
Prepared by: MJ			Checked by:	Checked by: PS Approved by: JPS			5
Date: August 24, 2012			Date: August 26, 2012 Date: August 27			′, 2012	

APPENDIX B.6

ONE-DIMENSIONAL CONSOLIDATION USING STANDARD LOAD INCREMENT (LIR)

(A Division of MEG Consulting Limited)

One-Dimensional Consolidation (ASTM D 2435)

011				W D 2100)				
Project:		Port of Anchorag	ge	Project No.: 12-MTS-009				
Location	n:	Anchorage, US				Date:	June 8, 2012	
Borehol	le:	BH-003-12				Station:	2	
Sample	No.:	ST-2				Depth (m):	28.29	
Weight of	of Ring (g):	216.64		Ring + Wet Weight (g):	383.68		Initial Void Ratio, e: 0.59	
Initial Hei	ight (mm):	25.40		Ring + Dry Weight (g):	353.98	H	leight of Soil, Hs (mm):	15.94
Diameter	r of Ring (mm):	63.50		Water Content (%):	21.6	H	eight of Void, Hv (mm):	9.46
Unit Weig	ght (kN/m³)	20.37		Specific Gravity, Gs:	2.72			
		Vertical	Height of	Vertical	Final	Change in	Coefficient of	Coefficient of
	Step	Stress	Sample	Strain	Void Ratio	Void Ratio	Compressibility	Volume Compressibility
	NO.	(kPa)	(mm)	(%)	e _f	e	a _v (m /win)	m _v (m /win)
	1	5	25.3746	0.1000	0.5915	0.00	0 4277	0.27
	2	35	25.1638	0.9300	0.5783	0.01	0.4377	0.27
	4	125	23.0300	2 1423	0.5704	0.01	0.2270	0.14
	5	250	24.6166	3.0841	0.5440	0.02	0.1200	0.08
	6	500	24.1932	4.7512	0.5174	0.03	0.1062	0.07
	7	1000	23.7651	6.4366	0.4906	0.03	0.0537	0.03
	8	1800	23.2228	8.5716	0.4566	0.03	0.0425	0.03
	9	3000	22.5742	11.1251	0.4159	0.04	0.0339	0.02
	0.65							
	0.60							
					•			
					•			
	0.55					•		
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tio,								
Ra						T T		
oid	0.50							
>								
	0.45						•	
	0.45							
	0.40							
	0.40							
	0.35							
1 10 100 1000					10000			
				Vert	ical Stress (kPa)			
Dronora	d Dur	κ.	IE	Chaokod D. "		200	Approved Dig	
Doto:	ы ву.	IV Iume 4	0 2012		F	0.2012	Data:	JF0
Dale.		June 1	0, 2012	Date.	June 1	3, 2012	Dale.	JUILE 19, 2012

Marine + Earth

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(A Division of MEG Consulting Limited)

Date:

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	June 8, 2012
Borehole:	BH-003-12	Station:	2
Sample No.:	ST-2	Depth (m):	28.29
Consolidation Step:	1	Vertical Stress (kPa):	4.8







(A Division of MEG Consulting Limited)









(A Division of MEG Consulting Limited)

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	June 8, 2012
Borehole:	BH-003-12	Station:	2
Sample No.:	ST-2	Depth (m):	28.29
Consolidation Step:	3	Vertical Stress (kPa):	70.0







(A Division of MEG Consulting Limited)

Date:

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	June 8, 2012
Borehole:	BH-003-12	Station:	2
Sample No.:	ST-2	Depth (m):	28.29
Consolidation Step:	4	Vertical Stress (kPa):	125.0







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One-Dimensional Consolidation (ASTM D 2435)







Marine + Earth **M E G** Geosciences

(A Division of MEG Consulting Limited)

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	June 8, 2012
Borehole:	BH-003-12	Station:	2
Sample No.:	ST-2	Depth (m):	28.29
Consolidation Step:	6	Vertical Stress (kPa):	500.0







(A Division of MEG Consulting Limited)

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	June 8, 2012
Borehole:	BH-003-12	Station:	2
Sample No.:	ST-2	Depth (m):	28.29
Consolidation Step:	7	Vertical Stress (kPa):	1000.0







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Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	June 8, 2012
Borehole:	BH-003-12	Station:	2
Sample No.:	ST-2	Depth (m):	28.29
Consolidation Step:	9	Vertical Stress (kPa):	3000.0





Marine +	Earth	
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One-Dimensional Consolidation (ASTM D 2435)

011									
Project:		Port of Anchora	age			Project No.:	12	-MTS-009	
Location	n:	Alaska				Date:	July 31, 2012		
Borehole	e:	BH-003-12				Station:		2	
Sample	No.:	ST-7				Depth (m):		35.36	
Weight of	Ring (g):	212.26		Ring + Wet Weight (g):	371.10		Initial Void Ratio, e:	0.76	
Initial Hei	ght (mm):	25.40		Ring + Dry Weight (g):	339.16	I	Height of Soil, Hs (mm):	14.47	
Diameter	of Ring (mm):	63.50		Water Content (%):	25.2	н	leight of Void, Hv (mm):	10.93	
Unit Weig	ıht (kN/m³)	19.37		Specific Gravity, Gs:	2.77				
	_	Vertical	Height of	Vertical	Final	Change in	Coefficient of	Coefficient of	
	Step	Stress	Sample	Strain	Void Ratio	Void Ratio	Compressibility	Volume Compressibility	
	NO. 1	(кРа)	(mm)	(%)	0 7551	e	a _v (117/1111)		
	2	35	25.3696	0.0400	0.7551	0.00	0 4707	0.27	
	3	70	25.0362	1.4321	0.7307	0.01	0.2920	0.17	
	4	125	24.8175	2.2935	0.7155	0.02	0.2750	0.16	
	5	250	24.4748	3.6423	0.6919	0.02	0.1895	0.11	
	6	500	23.9922	5.5425	0.6585	0.03	0.1335	0.08	
	7	1000	23.5013	10.3551	0.6246	0.03	0.0679	0.04	
	9	3000	22.2122	12.5504	0.5354	0.04	0.0321	0.02	
Void Ratio, e	0.80		•						
	0.55			100 Vert i	ical Stress (kPa	1000	•	10000	
Drogers	d Duu			Chaska - Div		20			
Prepare	и ву:			Dete:	ł	-5	Approved By:		
Date:		August	20, 2012	Date:	August	21,2012	Date:	August 27, 2012	

Marine + Earth

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(A Division of MEG Consulting Limited)

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	Jul 31, 2012
Borehole:	BH-003-12	Station:	#2
Sample No.:	ST-7	Depth (m):	35.36
Consolidation Step:	2	Vertical Stress (kPa):	







(A Division of MEG Consulting Limited)



(A Division of MEG Consulting Limited)



(A Division of MEG Consulting Limited)

One-Dimensional Consolidation (ASTM D 2435)

Project:	Port of Anchorage	Project No.:	12-MTS-009
Location:	Anchorage, US	Date:	Jul 31, 2012
Borehole:	BH-003-12	Station:	#2
Sample No.:	ST-7	Depth (m):	35.36
Consolidation Step:	5	Vertical Stress (kPa):	

Marine + Earth

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One-Dimensional Consolidation (ASTM D 2435)



Marine + Earth

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One-Dimensional Consolidation (ASTM D 2435)



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APPENDIX B.7

ONE-DIMENSIONAL CONSOLIDATION USING CONSTANT RATE OF LOADING (CRS)

(A Division of MEG Consulting Limited)

Marine + Earth **M E G**Geosciences



(A Division of MEG Consulting Limited)



Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	June 15	, 2012	
Borehole:	BH-001-12				Station:	CRS	#3	
Sample No.:	ST-4				Depth (m):	21.8	88	
Weight of Ring (g):	216.00		Ring + Wet Weight (g):	360.61		Initial Void Ratio, e:	1.00	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	326.05	F	leight of Soil, Hs (mm):	12.68	
Diameter of Ring (mm):	63.50		Water Content (%):	31.4	Н	eight of Void, Hv (mm):	12.72	
Unit Weight (kN/m³)	17.64		Specific Gravity, Gs:	2.74				
Loading Strain Rate (%/hr):		0.8	Max Stress (kPa):	2800	Backpro	essure (kPa):	414	
Unloading Strain Rate (%/h	r):	0.4	Max Strain (%):	11.85				

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	June 15	5, 2012	
Borehole:	BH-001-12				Station:	CRS	\$ #1	
Sample No.:	ST-7				Depth (m):	23.	69	
Weight of Ring (g):	211.63		Ring + Wet Weight (g):	371.05		Initial Void Ratio, e:	0.75	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	338.49		Height of Soil, Hs (mm):	14.51	
Diameter of Ring (mm):	63.50		Water Content (%):	25.7		Height of Void, Hv (mm):	10.89	
Unit Weight (kN/m ³)	19.44		Specific Gravity, Gs:	2.76				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	oressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	July 10,	2012	
Borehole:	BH-001-12				Station:	CRS	#1	
Sample No.:	ST-13				Depth (m):	29.1	14	
Weight of Ring (g):	216.64		Ring + Wet Weight (g):	379.02		Initial Void Ratio, e:	0.71	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	345.58	Не	eight of Soil, Hs (mm):	14.86	
Diameter of Ring (mm):	63.50		Water Content (%):	25.9	Не	ight of Void, Hv (mm):	10.54	
Unit Weight (kN/m ³)	19.80		Specific Gravity, Gs:	2.74				
Loading Strain Rate (%/hr)):	0.8	Max Stress (kPa):	7000	Backpre	ssure (kPa):	414	
Unloading Strain Rate (%/h	hr):	0.4	Max Strain (%):	14.9				

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Constant Rate of Strain Consolidation (ASTM D4186)

Constant Rate	of Strain Conso	lidatior	n (ASTM D4186)				Geosciences
Project:	Port of Anchorage				Project No.:	12-N	- ITS-009
Location:	Anchorage, US				Date:	July '	10, 2012
Borehole:	BH-001-12				Station:	CF	RS #1
Sample No.:	ST-15				Depth (m):	3	0.94
Weight of Ring (g):	215.97		Ring + Wet Weight (g):	381.49		Initial Void Ratio, e:	0.59
Initial Height (mm):	25.40		Ring + Dry Weight (g):	354.73	Не	eight of Soil, Hs (mm):	15.93
Diameter of Ring (mm):	63.50		Water Content (%):	19.3	Hei	ight of Void, Hv (mm):	9.47
Unit Weight (kN/m³)	20.19		Specific Gravity, Gs:	2.75			
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	7000	Backpres	ssure (kPa):	414
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	10.3			

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Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	May 29	, 2012	
Borehole:	BH-003-12				Station:	CRS	#3	
Sample No.:	ST-2				Depth (m):	28.	29	
Weight of Ring (g):	216.65		Ring + Wet Weight (g):	380.64		Initial Void Ratio, e:	0.63	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	350.64	H	leight of Soil, Hs (mm):	15.55	
Diameter of Ring (mm):	63.50		Water Content (%):	22.4	н	eight of Void, Hv (mm):	9.85	
Unit Weight (kN/m³)	20.00		Specific Gravity, Gs:	2.72				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpre	essure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	10.26				



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Date:	,		June 1	, 2012				Date:			July 1	2, 20)12			Date:		July	12, 2012	
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Loading	Strain Rat	te (%/	hr):	0	.8			Max Stress (kPa	a):	28	00			Back	pressu	ire (kPa):			414	
Unit Wei	ight (kN/m ³	3)	20.00					Specific Gravity	, Gs:	2.3	72									
Diameter	r of Ring (mm):	63.50					Water Conten	t (%):	22	.4				Height	of Void, Hv (m	m):		9.85	
Initial He	eight (mm)	:	25.40					Ring + Dry Weigh	ıt (g):	350	.64				Height	of Soil, Hs (m	m):		15.55	
Weight o	of Ring (g)	:	216.65					Ring + Wet Weigh	nt (g):	380	.64	1- 0			Ini	itial Void Ratio	, e:	-	0.63	
Sample	ə No.:		ST-2									De	epth	 (m):			2	8.29		
Boreho	n. de:		BH-003-12									St	atior	n [.]			CF	29, 201 RS #3	2	
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Constant Rate of Strain Consolidation (ASTM D4186)

			•	-				
Project:	Port of Anchorage				Project No.:	12-MTS-	-009	
Location:	Anchorage, US				Date:	May 29, 2	2012	
Borehole:	BH-003-12				Station:	CRS #	#2	
Sample No.:	ST-3				Depth (m):	29.20)	
Weight of Ring (g):	200.00		Ring + Wet Weight (g):	370.49		Initial Void Ratio, e:	0.64	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	332.83		Height of Soil, Hs (mm):	15.48	
Diameter of Ring (mm):	63.50		Water Content (%):	28.4		Height of Void, Hv (mm):	9.92	
Unit Weight (kN/m³)	20.79		Specific Gravity, Gs:	2.71				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	pressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	15.67				



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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MTS	-009	
Location:	Anchorage, US				Date:	May 29,	2012	
Borehole:	BH-003-12				Station:	CRS	#2	
Sample No.:	ST-3				Depth (m):	29.20	0	
Weight of Ring (g):	200.00		Ring + Wet Weight (g):	370.49		Initial Void Ratio, e:	0.64	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	332.83		Height of Soil, Hs (mm):	15.48	
Diameter of Ring (mm):	63.50		Water Content (%):	28.4		Height of Void, Hv (mm):	9.92	
Unit Weight (kN/m ³)	20.79		Specific Gravity, Gs:	2.71				
Loading Strain Rate (%/hr)):	0.8	Max Stress (kPa):	2800	Backp	pressure (kPa):	414	
Unloading Strain Rate (%/h	hr):	0.4	Max Strain (%):	15.67				

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MTS	6-009	
Location:	Anchorage, US				Date:	May 29,	2012	
Borehole:	BH-003-12				Station:	CRS	#1	
Sample No.:	ST-4				Depth (m):	29.8	31	
Weight of Ring (g):	214.38		Ring + Wet Weight (g):	374.37		Initial Void Ratio, e:	0.74	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	341.74		Height of Soil, Hs (mm):	14.62	
Diameter of Ring (mm):	63.50		Water Content (%):	25.6		Height of Void, Hv (mm):	10.78	
Unit Weight (kN/m ³)	19.51		Specific Gravity, Gs:	2.75				
Loading Strain Rate (%/hr):		0.8	Max Stress (kPa):	2800	Backp	ressure (kPa):	414	
Unloading Strain Rate (%/hr):	0.4	Max Strain (%):	11.85				

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MTS-	009	
Location:	Anchorage, US				Date:	May 29, 2	2012	
Borehole:	BH-003-12				Station:	CRS #	1	
Sample No.:	ST-4				Depth (m):	29.81		
Weight of Ring (g):	214.38		Ring + Wet Weight (g):	374.37		Initial Void Ratio, e:	0.74	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	341.74		Height of Soil, Hs (mm):	14.62	
Diameter of Ring (mm):	63.50		Water Content (%):	25.6		Height of Void, Hv (mm):	10.78	
Unit Weight (kN/m³)	19.51		Specific Gravity, Gs:	2.75				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Back	kpressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Project:	Port of Anchorage				Project No.:	12-MT	S-009
Location:	Anchorage, US				Date:	June 1,	2012
Borehole:	BH-003-12				Station:	CRS	#1
Sample No.:	ST-5				Depth (m):	30.7	73
Weight of Ring (g):	214.38		Ring + Wet Weight (g):	363.77		Initial Void Ratio, e:	0.95
Initial Height (mm):	25.40		Ring + Dry Weight (g):	327.21	Hei	ight of Soil, Hs (mm):	13.00
Diameter of Ring (mm):	63.50		Water Content (%):	32.4	Hei	ght of Void, Hv (mm):	12.40
Unit Weight (kN/m³)	18.22		Specific Gravity, Gs:	2.74			
Loading Strain Rate (%/hr)):	0.8	Max Stress (kPa):	6940	Backpres	sure (kPa):	414
Unloading Strain Rate (%/	hr):	0.4	Max Strain (%):	23.5			



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Project:	Port of Anchorage				Project No.:	12-MTS	-009
Location:	Anchorage, US				Date:	Jun 1, 2	2012
Borehole:	BH-003-12				Station:	CRS	#1
Sample No.:	ST-5				Depth (m):	30.7	3
Weight of Ring (g):	214.38		Ring + Wet Weight (g):	363.77		Initial Void Ratio, e:	0.95
Initial Height (mm):	25.40		Ring + Dry Weight (g):	327.21	I	Height of Soil, Hs (mm):	13.00
Diameter of Ring (mm):	63.50		Water Content (%):	32.4	F	leight of Void, Hv (mm):	12.40
Unit Weight (kN/m³)	18.22		Specific Gravity, Gs:	2.74			
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	6940	Backpro	essure (kPa):	414
Unloading Strain Rate (%/h	ır):	0.4	Max Strain (%):	23.5			



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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MT	S-009
Location:	Anchorage, US				Date:	June 1,	2012
Borehole:	BH-003-12				Station:	CRS	#2
Sample No.:	ST-6				Depth (m):	31.	29
Weight of Ring (g):	211.63		Ring + Wet Weight (g):	365.62		Initial Void Ratio, e:	0.87
Initial Height (mm):	25.40		Ring + Dry Weight (g):	331.00		Height of Soil, Hs (mm):	13.61
Diameter of Ring (mm):	63.50		Water Content (%):	29.0		Height of Void, Hv (mm):	11.79
Unit Weight (kN/m³)	18.78		Specific Gravity, Gs:	2.77			
Loading Strain Rate (%/hr):		0.8	Max Stress (kPa):	6931	Back	pressure (kPa):	414
Unloading Strain Rate (%/h	ır):	0.4	Max Strain (%):	20.7			

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Project:	Port of Anchorage				Project No.:	12-MT	S-009
Location:	Anchorage, US				Date:	June 1,	, 2012
Borehole:	BH-003-12				Station:	CRS	#2
Sample No.:	ST-6				Depth (m):	31.2	29
Weight of Ring (g):	211.63		Ring + Wet Weight (g):	365.62		Initial Void Ratio, e:	0.87
Initial Height (mm):	25.40		Ring + Dry Weight (g):	331.00		Height of Soil, Hs (mm):	13.61
Diameter of Ring (mm):	63.50		Water Content (%):	29.0		Height of Void, Hv (mm):	11.79
Unit Weight (kN/m ³)	18.78		Specific Gravity, Gs:	2.77			
Loading Strain Rate (%/hr):		0.8	Max Stress (kPa):	6931	Backp	ressure (kPa):	527
Unloading Strain Rate (%/hr)):	0.4	Max Strain (%):	20.7			



		Effectiv	ve Stress (kPa)		
Prepared By:	PS	Checked By:	GF	Approved By:	JPS
Date:	June 4, 2012	Date:	July 12, 2012	Date:	July 12, 2012

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	June 11	, 2012	
Borehole:	BH-003-12				Station:	CRS	S #1	
Sample No.:	ST-7				Depth (m):	35.	33	
Weight of Ring (g):	215.99		Ring + Wet Weight (g):	376.52		Initial Void Ratio, e:	0.74	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	344.01		Height of Soil, Hs (mm):	14.59	
Diameter of Ring (mm):	63.50		Water Content (%):	25.4	I	Height of Void, Hv (mm):	10.81	
Unit Weight (kN/m ³)	19.58		Specific Gravity, Gs:	2.77				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	ressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	June 1,	2012	
Borehole:	BH-003-12				Station:	CRS	#3	
Sample No.:	ST-9				Depth (m):	38.3	30	
Weight of Ring (g):	216.69		Ring + Wet Weight (g):	382.13	Ir	nitial Void Ratio, e:	0.62	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	350.94	Heigh	t of Soil, Hs (mm):	15.64	
Diameter of Ring (mm):	63.50		Water Content (%):	23.2	Height	of Void, Hv (mm):	9.76	
Unit Weight (kN/m³)	20.18		Specific Gravity, Gs:	2.71				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	6932	Backpressu	re (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	16.0				



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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	June 1	, 2012	
Borehole:	BH-003-12				Station:	CRS	S #3	
Sample No.:	ST-9				Depth (m):	38.	.30	
Weight of Ring (g):	216.69		Ring + Wet Weight (g):	382.13		Initial Void Ratio, e:	0.62	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	350.94		Height of Soil, Hs (mm):	15.64	
Diameter of Ring (mm):	63.50		Water Content (%):	23.2	I	Height of Void, Hv (mm):	9.76	
Unit Weight (kN/m ³)	20.18		Specific Gravity, Gs:	2.71				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	6932	Backp	ressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	16.0				

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Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	June 5,	2012	
Borehole:	BH-003-12				Station:	CRS	#2	
Sample No.:	ST-10				Depth (m):	38.9	96	
Weight of Ring (g):	216.65		Ring + Wet Weight (g):	381.65		Initial Void Ratio, e:	0.59	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	348.30	He	eight of Soil, Hs (mm):	15.93	
Diameter of Ring (mm):	63.50		Water Content (%):	25.3	Hei	ight of Void, Hv (mm):	9.47	
Unit Weight (kN/m³)	20.12		Specific Gravity, Gs:	2.61				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpres	ssure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Date:		Ju	une 9	, 201	2		D	Date:		Ju	uly 1	2, 2	201	2	Date:			Jull	y 12	2, 20)12

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Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	Jun 05,	, 2012	
Borehole:	BH-003-12				Station:	CRS	\$ #1	
Sample No.:	ST-12				Depth (m):	40.4	48	
Weight of Ring (g):	214.38		Ring + Wet Weight (g):	376.89		Initial Void Ratio, e:	0.70	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	346.34	н	eight of Soil, Hs (mm):	14.94	
Diameter of Ring (mm):	63.50		Water Content (%):	23.1	Не	eight of Void, Hv (mm):	10.46	
Unit Weight (kN/m ³)	19.82		Specific Gravity, Gs:	2.79				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpre	essure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Constant Rate	of Strain Conso	olidatio	n (ASTM D4186)				Geosciences
Project:	Port of Anchorage				Project No.:	12-M	- 1TS-009
Location:	Anchorage, US				Date:	June	6, 2012
Borehole:	BH-003-12				Station:	CF	RS #3
Sample No.:	ST-15				Depth (m):	4	2.82
Weight of Ring (g):	211.63		Ring + Wet Weight (g):	371.55	I	Initial Void Ratio, e:	0.69
Initial Height (mm):	25.40		Ring + Dry Weight (g):	342.77	Heig	ht of Soil, Hs (mm):	15.06
Diameter of Ring (mm):	63.50		Water Content (%):	21.9	Heigh	nt of Void, Hv (mm):	10.34
Unit Weight (kN/m³)	19.50		Specific Gravity, Gs:	2.75			
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpress	ure (kPa):	414
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85			

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	June 8,	2012	
Borehole:	BH-003-12				Station:	CRS	#1	
Sample No.:	ST-16				Depth (m):	42.9	98	
Weight of Ring (g):	214.37		Ring + Wet Weight (g):	373.43		Initial Void Ratio, e:	0.77	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	339.23	н	eight of Soil, Hs (mm):	14.34	
Diameter of Ring (mm):	63.50		Water Content (%):	27.4	Не	eight of Void, Hv (mm):	11.06	
Unit Weight (kN/m ³)	19.40		Specific Gravity, Gs:	2.75				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpre	essure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				
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Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	June 2	0, 2012	
Borehole:	BH-004-12				Station:	CRS	S #2	
Sample No.:	ST-3				Depth (m):	19	.80	
Weight of Ring (g):	215.99		Ring + Wet Weight (g):	381.31		Initial Void Ratio, e:	0.62	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	350.77		Height of Soil, Hs (mm):	15.70	
Diameter of Ring (mm):	63.50		Water Content (%):	22.7	I	Height of Void, Hv (mm):	9.70	
Unit Weight (kN/m ³)	20.16		Specific Gravity, Gs:	2.71				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	ressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				



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Project:	Port of Anchorage				Project No.:	12-MT	S-009
Location:	Anchorage, US				Date:	June 21	1, 2012
Borehole:	BH-004-12				Station:	CRS	S #1
Sample No.:	ST-7				Depth (m):	24.	62
Weight of Ring (g):	211.27		Ring + Wet Weight (g):	373.75		Initial Void Ratio, e:	0.76
Initial Height (mm):	25.40		Ring + Dry Weight (g):	340.48		Height of Soil, Hs (mm):	14.42
Diameter of Ring (mm):	63.50		Water Content (%):	25.8	I	Height of Void, Hv (mm):	10.98
Unit Weight (kN/m³)	19.82		Specific Gravity, Gs:	2.83			
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	ressure (kPa):	414
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85			



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Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	June 21	, 2012	
Borehole:	BH-004-12				Station:	CRS	#1	
Sample No.:	ST-7				Depth (m):	24.0	62	
Weight of Ring (g):	211.27		Ring + Wet Weight (g):	373.75		Initial Void Ratio, e:	0.76	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	340.48	H	leight of Soil, Hs (mm):	14.42	
Diameter of Ring (mm):	63.50		Water Content (%):	25.8	н	eight of Void, Hv (mm):	10.98	
Unit Weight (kN/m ³)	19.82		Specific Gravity, Gs:	2.83				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpr	essure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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June 25, 2012

Constant Rate of Strain Consolidation (ASTM D4186)

June 23, 2012

Date:

Date:



June 25, 2012

Date:

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Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	June 23	, 2012	
Borehole:	BH-004-12				Station:	CRS	#3	
Sample No.:	ST-9				Depth (m):	27.6	67	
Weight of Ring (g):	211.62		Ring + Wet Weight (g):	370.32		Initial Void Ratio, e:	0.77	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	336.29		Height of Soil, Hs (mm):	14.37	
Diameter of Ring (mm):	63.50		Water Content (%):	27.3		Height of Void, Hv (mm):	11.03	
Unit Weight (kN/m³)	19.35		Specific Gravity, Gs:	2.74				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	oressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	July 17,	, 2012	
Borehole:	BH-004-12				Station:	CRS	#2	
Sample No.:	ST-11				Depth (m):	29.2	26	
Weight of Ring (g):	211.95		Ring + Wet Weight (g):	373.48		Initial Void Ratio, e:	0.70	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	342.04	н	leight of Soil, Hs (mm):	14.94	
Diameter of Ring (mm):	63.50		Water Content (%):	24.2	Н	eight of Void, Hv (mm):	10.46	
Unit Weight (kN/m ³)	19.70		Specific Gravity, Gs:	2.75				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	7000	Backpre	essure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	17.47				

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Project:	Port of Anchorage				Project No.:	12-MTS	S-009	
Location:	Anchorage, US				Date:	July 11,	, 2012	
Borehole:	BH-004-12				Station:	CRS	#2	
Sample No.:	ST-13				Depth (m):	30.6	63	
Weight of Ring (g):	216.63		Ring + Wet Weight (g):	379.69		Initial Void Ratio, e:	0.75	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	348.03	н	leight of Soil, Hs (mm):	14.51	
Diameter of Ring (mm):	63.50		Water Content (%):	24.1	Н	eight of Void, Hv (mm):	10.89	
Unit Weight (kN/m ³)	19.89		Specific Gravity, Gs:	2.86				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	7000	Backpre	essure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	14.9				

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Constant Rate of Strain Consolidation (ASTM D4186)

Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	June 27	7, 2012	
Borehole:	BH-005-12				Station:	CRS	S #1	
Sample No.:	ST-3				Depth (m):	14.	83	
Weight of Ring (g):	211.27		Ring + Wet Weight (g):	375.42		Initial Void Ratio, e:	0.70	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	345.25		Height of Soil, Hs (mm):	14.95	
Diameter of Ring (mm):	63.50		Water Content (%):	22.5	I	Height of Void, Hv (mm):	10.45	
Unit Weight (kN/m ³)	20.02		Specific Gravity, Gs:	2.83				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backp	ressure (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				



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Project:	Port of Anchorage				Project No.:	12-MT	S-009	
Location:	Anchorage, US				Date:	July 5,	2012	
Borehole:	BH-005-12				Station:	CRS	#2	
Sample No.:	ST-11				Depth (m):	22.5	53	
Weight of Ring (g):	216.64		Ring + Wet Weight (g):	380.99	In	itial Void Ratio, e:	0.73	
Initial Height (mm):	25.40		Ring + Dry Weight (g):	348.47	Height	of Soil, Hs (mm):	14.71	
Diameter of Ring (mm):	63.50		Water Content (%):	24.7	Height	of Void, Hv (mm):	10.69	
Unit Weight (kN/m ³)	20.04		Specific Gravity, Gs:	2.83				
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpressur	e (kPa):	414	
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85				

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Date:

Constant Rate of Strain Consolidation (ASTM D4186)

Constant Rate	e of Strain Consc	olidatio	n (ASTM D4186)				Geosciences
Project:	Port of Anchorage				Project No.:	12-N	TS-009
Location:	Anchorage, US				Date:	July	5, 2012
Borehole:	BH-005-12				Station:	CF	RS #1
Sample No.:	ST-13				Depth (m):	2	4.31
Weight of Ring (g):	211.25		Ring + Wet Weight (g):	371.99		Initial Void Ratio, e:	0.75
Initial Height (mm):	25.40		Ring + Dry Weight (g):	341.26	Hei	ight of Soil, Hs (mm):	14.51
Diameter of Ring (mm):	63.50		Water Content (%):	23.6	Heig	ght of Void, Hv (mm):	10.89
Unit Weight (kN/m ³)	19.60		Specific Gravity, Gs:	2.83			
Loading Strain Rate (%/hr)	:	0.8	Max Stress (kPa):	2800	Backpres	sure (kPa):	414
Unloading Strain Rate (%/h	nr):	0.4	Max Strain (%):	11.85			

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